

3rd International Workshop on
*Plasma Edge
Theory in
Fusion
Devices*

Bad Honnef
Physikzentrum
22 - 24 June 1992

Abstracts

Zouhier ABOU-ASSALEH
INRS - énergie et Matériaux
AEA-Fusion, Culham

- 3rd International workshop on Plasma Edge Theory
Bad Honnef. 1992.
- Edge activities at LLNL and UCLA
- Review of Paper on "New Boundary conditions"
By Yu. L. Izgitkhanov et al
Presented at Bad Honnef 1992
- Fokker-Planck Modelling of edge Plasma
Near the Neutralizer Plate in a Tokamak
By: Z. ABOU-ASSALEH et al.
Presented at Bad Honnef 1992.

Review of Papers at the 3rd International Workshop on Plasma Edge Theory
Bad Honnef, Federal Republic of Germany. 92

Zouhier Abou-Assaleh, Ph.D., Culham Laboratory, Abingdon, Oxfordshire, UK. AEA Fusion

Forschungszentrum Jülich GmbH
Institute for Plasma Physics

3rd International Workshop on
Plasma Edge Theory
in Fusion Devices

Abstracts of the Papers Presented
Physikzentrum Bad Honnef, Germany
22 - 24 June 1992

The Workshop was jointly organized by the Forschungs-
zentrum Jülich and the Arbeitsgemeinschaft Plasma-
physik of the Universities of Bochum, Düsseldorf, Essen
and KFA Jülich.

June 1992



ENERGIE EN

2D

- R. Zanino : Finite element modelling of the
Garching-Torino scrape-off layer
- A. Taroni : The multi-fluid codes EDGE1D and
JET EDGE2D: Models and results
- K. Parbhakar & J. Lewendowski : Properties of a biased
INRS divertor scrape-off layer
plasma (1D)
- T. D. Rognlien, et al : A fully implicit, 2-D fluid
LLNL transport code for
simulating tokamak edge
plasma.

B2

- W. D. D'haeseleer, H. D. Pacher, G. W. Pacher

NET

B2 with an analytical recycling model for ITER/NET

- M. W. Wuttke et al.: Validation of the B2-EIRENE code by comparison with TEXTOR experiments
- H. Kastelewicz et al.: Parameter study of the divertor conditions in ASDEX-upgrade

B2, Analytical recycling, EIRENE (neutras)

- R. Schneider et al.: Extensions of B2 for the simulation of ASDEX-upgrade scrape-off layer plasma

- Deuterium plasma & Helium ions as impurity

- Neutral atoms and molecules:

Monte-carlo code EIRENE

- B2 plasma profiles \rightarrow calculates the source terms

- B2-EIRENE more realistic recycling model than the stand-alone B2-code.

Kinetic

- Krasheninnikov et al.
 - Kinetic modeling of the transport processes in the tokamak edge plasma. (Preliminary results).
 - Electron Heat conduction and supra-thermal particles
- R. Chodura (Garching)
 - Kinetic effects in the scrape-off layer
 - Non-Maxwellian: 1 - sources: from the bulk plasma
Reionized recycled neutral
 - 2 - Parallel transport
 - 3 - sheath
- Z. ABOU-ASSALEH et al.
 - Fokker-Planck Modelling of edge plasma near the Neutralizer plate in a tokamak.
 - * electron kinetic / ion fluid

UCLA

R.W. Conn } PISCES (D₁, D₁₁)
F. Najmabadi } 1D & 2D Modelling
Y. HIROOKA }
B. Merriman } UCLA next-generation code

LLNL

T. D. Rognlien
M. E. Reink
G. D. Porter
⋮

2D code - LEDGE

Fully implicit
2D fluid

Applications: DIII-D



Effective Boundary Conditions at the Plasma-surface interface.

YU. L. Igitkhanov, A.M. RUKNOV

Presented at the 3rd international workshop on plasma edge theory in Fusion Devices, Bad Honnef, Germany 1992.

- *Fluid can be used if the nonlocal effects are included into the transport coefficients and the appropriate boundary conditions are present.*
- *The existing boundary conditions do not permit to include the contribution of suprathermal particles due to their local nature.*
- *New Boundary conditions for fluid models of SOL and divertor plasma:*

New Boundary conditions

- starting from BGK kinetic equation
- This boundary conditions permit to extend the applicability of fluid equations to the moderate collisionality regimes typical for the divertor plasma.
- The BGK approximation gives an opportunity to express the boundary fluxes as functions of fluid profiles instead of local values
- Used $T_i = 0$:
 - The Boundary conditions effects by
 - whole ion distribution function
 - Hot tail of the electron distribution function.

Kinetic Model

1D along \vec{B}

e-e collisions presented by the BKG approximation

e-n collisions



$$f_M(n_s, T_s) = \psi_s$$

$$v_x \frac{\partial F}{\partial x} = \nu_m (n \psi_m - F) + 0.5 n \nu_n \delta(|v_x| - v_0) \delta(v_y) \delta(v_z) \\ - \nu_n F + \nu_s n_s \psi_s \mathcal{V}(-|x| + a) - F \nu_s$$

$1/\nu_m$ is the Maxwellization time

F is the electron distribution function

ψ_s is the Maxwellian

ψ_m is the local shifted Maxwellian

ν_n is the frequency of ionisation

$$\nu_s = N \langle \sigma v \rangle, \quad N(x) = N_w \exp(-|x|/\lambda - t/\tau)$$

Boundary conditions at the entrance of the Debye sheath:

- Mirror reflection for the particles with energy below a potential barrier
- Φ_d the sheath drop is found from the local parameters of ϕ_m , n , T , and v

New variables

$$\xi = \frac{x}{L}, \quad u = \frac{v_x}{v_s}, \quad \tilde{T} = \frac{T}{T_s}, \quad \tilde{v} = \frac{v}{v_s}$$

The solution of the kinetic equation:

$$f^+(u, \xi) = \exp\left[-\int_{-1}^{\xi} \frac{d\xi'}{u}\right] \int_{-1}^{\xi} \frac{R(\xi')}{u} \exp\left[+\int_{-1}^{\xi'} \frac{d\xi''}{u\tilde{v}}\right] d\xi' + C(u) \exp\left[-\int_{-1}^{\xi} \frac{d\xi'}{u\tilde{v}}\right]$$

where

$$1/\tilde{v} = \nu_m + \nu_n + \nu_s$$

$$R(\xi') = \frac{n}{\sqrt{\pi T}} \nu_m \exp[-(u - v^2)/T] + \nu_s \frac{\mathcal{Q}(-|k| + a)}{\sqrt{\pi}} \exp(-u^2) + 0.5 n \nu_n \delta(|u| - u_0)$$



+ : half space of positive velocities

$C(u)$: mirror reflection from the wall.

Fluid Model

Set of fluid equations: particles, energy, and momentum
with sink and source terms

Boundary conditions:

at $\eta = 0$ (symmetry plane): $j|_0 = 0$, $\frac{\partial T}{\partial \eta}|_0 = 0$

at $\eta = 1$ (plate): The particle, momentum and heat
flux values are obtained by
integration of $f^+(u, \eta)$

Profiles obtained by iteration

Boundary conditions at the plate with the
profiles of hydrodynamic quantities T, v, n
and to include kinetic effects into the
fluid approach.

Improvement of the transport coefficients by including the nonlocal effects

Heat flux

$$\left(\nu + \frac{8}{3} \frac{\partial u}{\partial f} \right) q = \alpha \nu_m q_{SH} + \frac{5}{3} u P \frac{\partial u}{\partial f} - (R u - Q)$$

where: $\nu = \nu_m + \nu_s + \nu_n$

u is the fluid velocity

$$P = n T$$

R and Q are the integrals over f_e with the weight of \bar{v}^2 and $v^2 v_x$

q_{SH} is the classical expression

Viscosity

$$\pi = - \frac{4}{3 \nu_m} n T 0.73 \left[\frac{\partial v}{\partial f} + \frac{2}{5} \frac{1}{n T} \frac{\partial q}{\partial f} \right]$$

q is the thermal conduction flux.

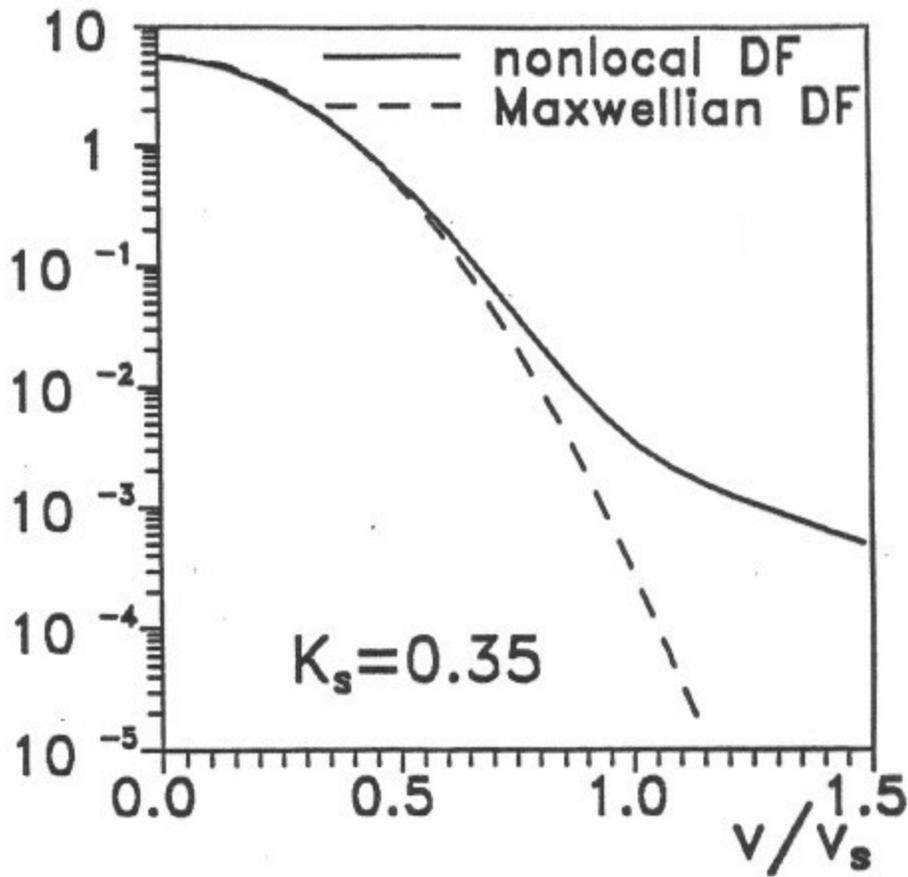


Fig.1 The comparison of the boundary distribution functions, corresponding to the nonlocal boundary conditions with the Maxwellian one

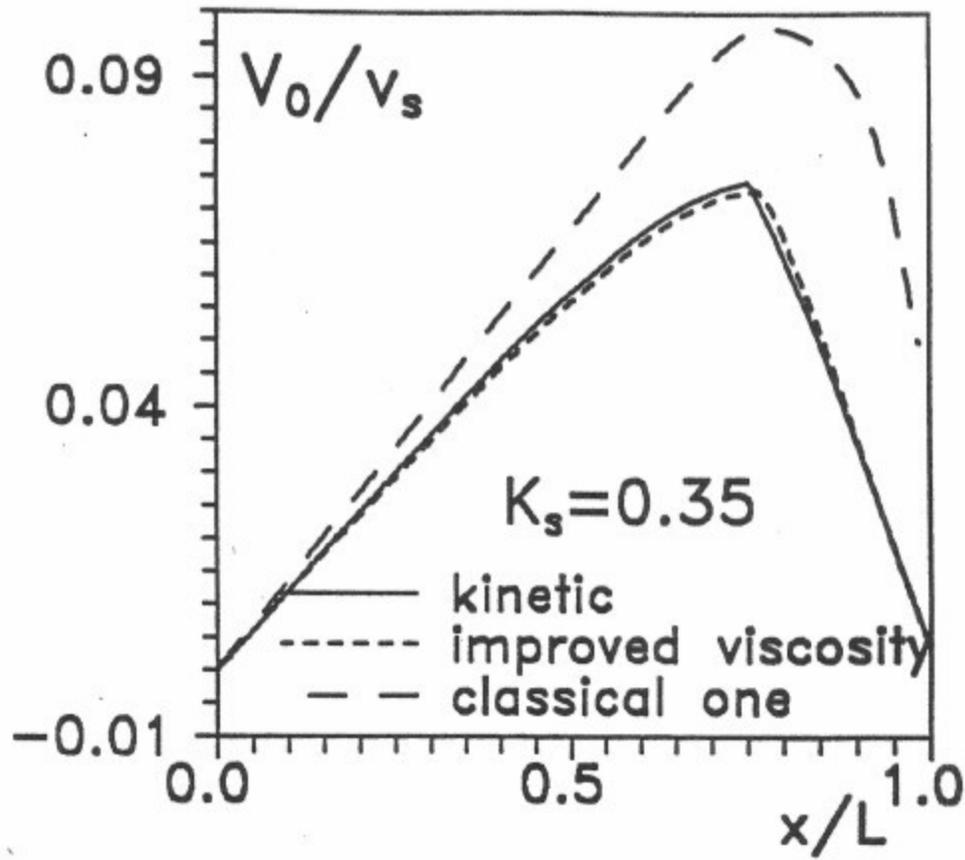


Fig.2 The velocity profiles corresponding to the classical viscosity, the improved one and the result of kinetic treatment

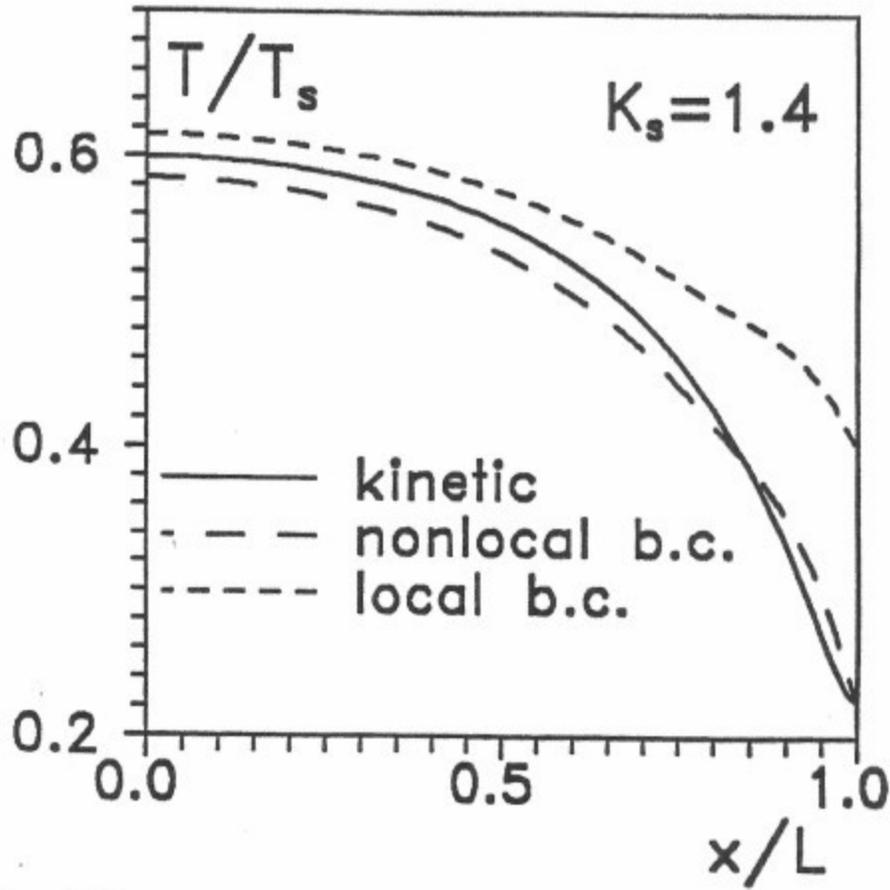


Fig.3 The temperature profiles for three cases: kinetic, local and nonlocal boundary conditions

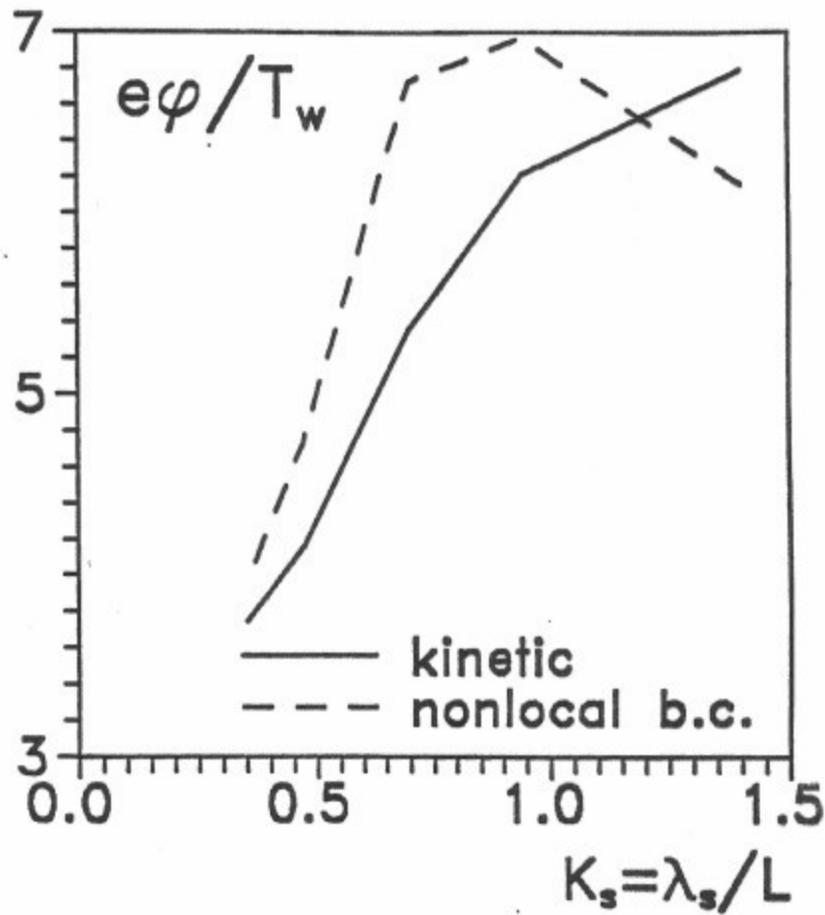


Fig.4 The sheath potential drop vs $K_s = \lambda_s/L$, where λ is electron mean free path and L is the length of magnetic field line

Conclusions.

1. The effective boundary conditions for the fluid set of equation at the plasma surface interface, which include the kinetic effects, are suggested.

2. The BGK approximation gives an opportunity to express the boundary fluxes as functionals of fluid profiles instead of local values.

3. The comparison with the kinetic solution shows that the proposed boundary conditions give such an accuracy of plasma parameters at the plate which is provided by the proximity of fluid profiles to the kinetic ones, i.e. the contribution of suprathermal particles in the transport coefficients is taken into account.

4. The conventional viscosity term does not allow one to obtain the velocity profiles close to the kinetic ones. It has been shown that the usage of a viscous term from the 13 - moment Grad approximation, taking account of a heat flux contribution, is more adequate to represent the regimes of moderate collisionality.

5. The flux - limited classical electron heat conduction does not bring to satisfactory results. The expression for a thermal heat flux in terms of higher moments of distribution function, could be recommended for the fluid codes.

$$\left. \begin{matrix} j \\ \pi \\ q \end{matrix} \right\} = \int G(\mathcal{E}, n, T, V) dW$$